

STRUCTURAL ANALYSIS OF CORN SILO BY COMPUTING VERTICAL AND LATERAL FORCES

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Abstract: Grainy products cause to pressures at horizontal and vertical directions in bottom floor and the walls of silos. The forces applied to silos from the grains depend upon the mostly moisture content, frictions and thermal expansions. This study focuses on the fact that the product formed by the stored granular products has semi fluid property for the calculation of the pressures. The loads act on a corn silo; lateral design pressures, static vertical pressure and vertical frictional forces were calculated. The structural strength of the designed corn silo was analyzed with FEA (Finite Element Analysis) methods using Ansys Workbench Static Structural Tool. Janssen's equations were used for lateral design pressures and vertical fixed surfaces were defined in the analysis environment. The mechanical safety of the design and appropriateness of the selected material for the structure (S 235 Steel) were checked. The occurred maximum stress, strain, deflection and safety factor were obtained as 123.6MPa, 0.089 %, 0.47mm and 1.9, respectively for critical regions. The results from the analysis showed that the designed system was mechanically safe enough to store 15 tones corn within the volume of 46.2m3
Key words: Corn Silo Design, Finite Element Analysis, High Silos, Loads Act on silo

1. INTRODUCTION

Silos are widely used in many different industries for storing and preventing a huge range of different solids. The capacities of them can vary a few tones to thousands of tones [1]. The design types of the silos vary so much; however, they are generally built in industrial locations. In farm industry for grain storage, there are standard silo products commercially are cost effective available which and functional. In other industries such as cement and mineral storage very large silos are used and each silo must be individually designed for the special conditions. Each silo is normally designed to contain a limited material and usage for different materials may cause to damage. As each bulk solid has its individual properties, storage of different one cause to the damages.

Silos can be constructed of steel or reinforced concrete. Steel bins range from heavily stiffened flat plate structures to efficient unstiffened shell structures. They can be supported on columns, load bearing skirts or be hung from floors. Flat bottom bins are usually supported directly on foundation. There are also two types of silos named as hopper and truck load [2]. Different types of silos are shown in Figure 1.

The structural strength of these components must be taken into consideration in the design stage. Although small sizes of silos do not present significant structural problems, large silos may cause to varied situations that many different aspects need special attention.

1.1. Loads act on Silos

Storage and discharge loads in silos depend on different conditions such as stored material and its propensity to cohesion, deposition method, potential for segregation and geometry of container [3].

The most comprehensive design standard for these loads is EN 1991-4 (2006), with the name

of "Actions on structures, Part 4: Silos and tanks". In this standard, different classes of silos are defined by the mean of size, aspect ratio, wall roughness and construction material, this

standard also defines the properties that must be considered for the stored solids and different loading conditions for the design calculations[4].



Fig. 1. Different types of silos (a) Flat bottom (b) Hopper (c) Truck load)

1.2. Product Loads

Grain products have semi-fluid properties. Therefore, they try to push the storage walls by applying horizontal and vertical pressure. Grain products cause pressure on storage walls like liquids. The applied horizontal pressure is zero at the top of the granular products stack, and at the bottom of the silo is the maximum level due to the pressure of the whole product. The vertical pressure in storage occurs from friction between the product and the silo walls [5].

The horizontal and vertical pressure caused by the product stored in the silo is calculated by using different equations

according to the high and low state of the silo. The height (h) of the product at the storage is compared with the storage hydraulic radius (r). If h< R, it is accepted as low grain storage and if h> R, it is high grain storage as shown in Figure 2 [6].



Fig. 2. Storage system characteristics in granular product silo (a) Low Grain Storage (b) High Grain Storage

1.2.1. Rankine approach

If there is a situation that the horizontal pressure increases linearly with the height of the stack in low tanks, it is more convenient to use the classical Rankine equation [7].

1.2.2. Janssen approach

The increase in the horizontal pressure in the high grain storage due to the stack height is less than the linear increase in the horizontal pressure in the low grain storage due to the stack height. For this purpose, it is more convenient to use the Janssen equation for the calculations of the horizontal pressure [8].

2. DESIGN OF SILO

In the mechanical design process; several issues were taken into account such as compact size, sufficient stiffness and toughness, management of time and cost.

The silo was prepared using parametric solid modelling technique using Autodesk Inventor software as shown in Figure 3.



Fig. 3. Design of Silo

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S235 steel is commonly used in engineering applications due to its easy process ability and low cost.

Mechanical properties of the S235 steel materials are given in Table 1.

	Table 1
Mechanical Properties of S235 Steel	

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Parameters	Value		
Yield-Tensile Strength (MPa)	235		
Elastic Modulus (GPa)	160		
Poisson's Ratio	0.3		
Density (g/cm ³)	7.85		

3. MATERIAL AND METHOD

3.1. Calculation of Loads

The silo height (h) and the hydraulic radius (R) values were about 6.8 and 1.5 meters, respectively. According to these values, the silo was assumed high grain storage and Janssen approach was applied.

Static vertical pressures at any depth were calculated by using Equation 1.

$$P_{\nu} = \frac{R \times W \times \left[1 - e^{\frac{\mu \times k \times Y}{R}}\right]}{\mu \times k} \tag{1}$$

Where;

 P_{ν} Vertical pressure exerted by the stored granular corn material (kg/m²)

- *R* Hydraulic radius (m)
- W Weight of the stored material (kg/m^3)
- *k* Lateral-to-vertical pressure ratio
- μ Coefficient of friction between the stored corn material and the bin wall

Y Depth of grain mass from the level or sloping surface usually from the centroid of conical grain mass to the point where the bin loads are to be calculated, (m)

 C_d Over-pressure coefficient

Lateral static pressures were calculated by using Equation (2);

$$P_{h} = P_{v} \times k \tag{2}$$

Then, the lateral design pressures were calculated by using Equation (3);

$$L_d = P_h \times C_d \tag{3}$$

The grain pressures normal to sloping surfaces, F_n were calculated by using Equation (4);

$$F_n = P_v \times \cos^2 \psi + L_d \times \sin^2 \psi \tag{4}$$

Where, ψ was the angle of sloping part from horizontal plane (degrees).

Vertical friction forces on the vertical sections of corrugations were calculated by using Equation (5);

$$V_{w} = L_{d} \times \mu \tag{5}$$

Friction forces on sloping sections of corrugations were calculated by using Equation (6);

$$V_f = F_n \times \mu \tag{6}$$

3.2. Structural Analysis

Structural analysis was applied to get strength information of the silo with Finite Element Analysis (FEA) approach using Ansys Workbench Static Structural tool.

The pressure loads obtained from the load calculations were used as input for the analysis. Meshed view of the structural model with Ansys Workbench Static Structural Analysis is shown in Figure 4.



Fig. 4. Mesh view of silo

4. RESULTS AND DISCUSSION

4.1. Calculated Loads

The calculated pressure loads caused from granular corn are given in Table 2 and Figure 5.

Loads in sub calcillation	Loads	in	silo	calculation
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Table 2.

Loads	Values
	(MPa)
Static vertical pressure (P _v)	0.0199
Lateral static pressure (P _h)	0.0080
Lateral design pressure (L _d)	0.0115
Grain pressures normal to sloping	0.0150
surfaces (F _n)	
Vertical friction forces on the vertical	0.0023
sections (V _w)	
Friction forces on sloping sections	0.0030
(V _f)	
Horizontal lateral design pressure	0.0088
(L_{dx})	

Vertical lateral design pressure (L_{dy}) 0.0074

4.2. Analysis Results

Static analysis results (equivalent stress, strain and safety factor) for different components of the corn silo (leg, walls, top and bottom) are given in Table 3 and Figure 6.

Table 3.

Static a	analysis	results
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	Equivalent Stress (MPa)	Equivalent Strain (%)	Safety Factor
Leg	123.6	0.089	1.90
Wall 1	56	0.038	4.08
Wall 2	57.7	0.038	4.08
Wall 3	57.7	0.038	4.08
Wall 4	57.7	0.039	4.08
Тор	22.6	0.014	10.41
Bottom	94.6	0.075	2.48

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	FILE	BREAKPOINTS	RUN	Static vertical pressure everted by the stored ou	^ 🖸 Cd 🔹 ^
Silo.m*	x			Du= 0.0199 N/mm^2	.a. En
1 -	clear, clc		^ L	1 0.0155 N/Add 2	Ldx
2 -	R=1.465;	%Hydraulic radius		Lateral static pressure	Ldy
3 -	₩=720;	%Weight of the stored mater	ial	Ph= 0.0080 N/mm^2	H Mu
4 -	Mu=0.20;	&Coefficient of friction be	tween the stored c		Psi Pri
5 -	k=0.4;	&Lateral-to-vertical pressu	are ratio	Lateral design pressure	Pv
6 -	Y=3.061;	&Depth of grain mass		$Ld= 0.0115 \text{ N/mm}^2$	H R
7 -	Cd=1.45;	%Over-pressure coefficient			UT VW
8 -	Psi=50;	<pre>%Angle of sloping part from</pre>	n horizontal plane	Grain pressures normal to sloping surfaces	W
9				Fn= 0.0150 N/mm^2	Y v
10 -	Pv=((R*W*(1-	exp((-Mu*k*Y)/R)))/(Mu*k))*((9.80*10^-6);		< >
11 -	Ph=Pv*k;			Vertical friction forces on the vertical sections	Command His 💿
12 -	Ld=Ph*Cd;			Vw= 0.0023 N/mm^2	-Silo ^
13 -	Fn=Pv*cosd(P	<pre>si)^2+Ld*sind(Psi)^2;</pre>			-Gear c
14 -	Vw=Ld*Mu;			Friction forces on sloping sections	-silo
15 -	Vf=Fn*Mu;	e.		Vf= 0.0030 N/mm^2	-Copr c
16 -	Ldx=Ld*sind(Psi);			Gear_C
17 -	Ldy=Ld*cosd (Psi);		Vertical lateral design pressure	-5110
18				Ldx= 0.0088 N/mm^2	≝-≋ 2.07
19					⊢Silo
20 -	fprintf('Cal	culation of granular corn ma	terial loads in si	Horizontal lateral design pressure	-% 3.07
21 -	fprintf('Sta	tic vertical pressure exerte	ed by the stored gr	Ldy= 0.0074 N/mm^2	-% 3.07
22 -	fprintf('Pv=	<pre>%4.4f N/mm^2\n\n', Pv);</pre>			⊟-% 4.07
23 -	fprintf('Lat	eral static pressure\n');	~	fx >>	v −Silo v
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		script	Ln 16 Col 18		

Fig. 5. Pressure load calculation

A: Static Structural **Equivalent Stress** Type: Equivalent (von-Mises) Stress Unit: MPa Time: 1 4.07.2018 17:40 123,64 Max 109,9 96,165 Min 82,428 68,691 54,954 41,217 27,481 13,744 0,0070329 Min

Fig. 6. Structural analysis results

It can be understood from the analysis results that the maximum stress occurred on the leg of the silo (critical region). It was an expected result as the total pressure of the corn and silo affected on the legs. The strain, deflection and safety factor values were also obtained as 0.089 %, 0.47 mm and 1.9, respectively for critical regions. The analysis results showed that the designed system was mechanically safe enough to store 15 tones corn within the volume of 46.2 m^3 .

5. CONCLUSION

In this study, mechanical strength of a corn silo with the capacity of 15 tones and manufactured by S 235 steel was analyzed using the calculated pressure loads and FEA methods. From the results, the following conclusions can be withdrawn;

- 1) The safety factor was 1.9 with the material of S 235 steel.
- 2) The maximum stress was observed on the legs with the value of 123.6 MPa as it was expected.

3) The deflection was found as about 0.5 mm and it was a negligible value for the silo with the volume of 46.2 m^3 .

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ANALIZA STRUCTURALĂ A CORN SILO PRIN CALCULUL FORȚEI VERTICALE ȘI LATERALE

Rezumat: Produsele din cereale cauzează presiuni în direcții orizontale și verticale în subsolul fundului și pereții silozurilor. Forțele aplicate silozurilor din granule depind de conținutul de umiditate, fricțiunile și dilatările termice. Acest studiu se concentrează asupra faptului că produsul format de produsele granulare stocate are o proprietate semi-lichidă pentru calcularea presiunilor. Sarcinile acționează asupra unui siloz de porumb; presiunile laterale de proiectare, presiunea verticală statică și forțele de frecare verticale au fost calculate. Rezistența structurală a silozului de porumb proiectat a fost analizată prin metodele FEA (Element de analiză finită) folosind Ansys Workbench Structural Structural Tool. Ecuațiile lui Janssen au fost utilizate pentru presiuni de proiectare laterale și forțe verticale, deoarece înălțimea silozului proiectat a fost mai mare decât diametrul acestuia. Sarcini calculate și suprafețe fixe au fost definite în mediul de analiză. Sa verificat siguranța mecanică a designului și a caracterului adecvat al materialului selectat pentru structura (S 235 Steel). Stresul maxim, presiunea, deformarea și factorul de siguranță au fost obținute ca 123,6MPa, 0,089%, 0,47mm și respectiv 1,9 pentru regiunile critice. Rezultatele analizei au arătat că sistemul proiectat a fost suficient de sigur din punct de vedere mecanic pentru a stoca 15 tone de porumb în volumul de 46,2 m3

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