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DIRECT KINEMATICS MODELING OF TRTRR SERIAL MODULAR ROBOT

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Abstract: There is a modular serial robot noted TRTRR with two translation modules and three rotational modules, and that is inside the manufacturing cell. In this paper is presented the kinematics modeling using matrix study. For the five modules are given step by step the position matrix and the final result if they work as an assembly. In this paper there is the direct kinematics modeling and this is the continuing of the geometric modeling of the TRTRR robot.

Keywords: direct kinematics modeling, TRTRR robot, serial modular robot.

1. INTRODUCTION

The robot kinematics diagram type industrial TRTRR, is shown in figure 1. This is made up of the following: The vertical translation module 1 (MTV), module 2 of robot arm rotation (MRB), the module 3 for translation in the horizontal direction (MT), module 4 for the horizontal rotation (MR), the guidance module 5 (MO) of the prehensile tool noted 6.

2. DIRECT KINEMATICS MODELING

After shaping the robot direct geometric TRTRR as shown in Figure 1, has been obtained from the vector column of the operational coordinates.

Homogeneous transformation matrixes can be determined using the rotation matrixes and of position vectors obtained in geometric modeling. These matrixes of homogeneous transformation are set out below, in accordance with [Pop78], [Gui10e] and [ISP04]:

$$[T]_1^0(t) = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & l_1 + q_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}; [T]_2^1(t) = \begin{bmatrix} cq_2 & -sq_2 & 0 & 0 \\ sq_2 & cq_2 & 0 & 0 \\ 0 & 0 & 1 & l_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}; \quad (1)$$

$$[T]_3^2(t) = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & l_4 + q_3 \\ 0 & 0 & 1 & l_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}; [T]_4^3(t) = \begin{bmatrix} cq_4 & 0 & sq_4 & 0 \\ 0 & 1 & 0 & l_5 \\ -sq_4 & 0 & cq_4 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}; \quad (2)$$

$$[T]_5^4(t) = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & cq_5 & -sq_5 & l_6 \\ 0 & sq_5 & cq_5 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}; [T]_6^5(t) = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & l_7 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}; \quad (3)$$

$$[T]_2^0(t) = \begin{bmatrix} cq_2 & -sq_2 & 0 & 0 \\ sq_2 & cq_2 & 0 & 0 \\ 0 & 0 & 1 & l_1 + l_2 + q_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}; \quad (4)$$

$$[T]_3^0(t) = \begin{bmatrix} cq_2 & -sq_2 & 0 & -(l_4 + q_3)sq_2 \\ sq_2 & cq_2 & 0 & (l_4 + q_3)cq_2 \\ 0 & 0 & 1 & l_1 + l_2 + l_3 + q_1 \\ 0 & 0 & 0 & 1 \end{bmatrix};$$

$$[T]_4^0(t) = \begin{bmatrix} cq_2cq_4 & -sq_2 & cq_2sq_4 & -(l_4 + l_5 + q_3)sq_2 \\ sq_2cq_4 & cq_2 & sq_2sq_4 & (l_4 + l_5 + q_3)cq_2 \\ -sq_4 & 0 & cq_4 & l_1 + l_2 + l_3 + q_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}; \quad (5)$$

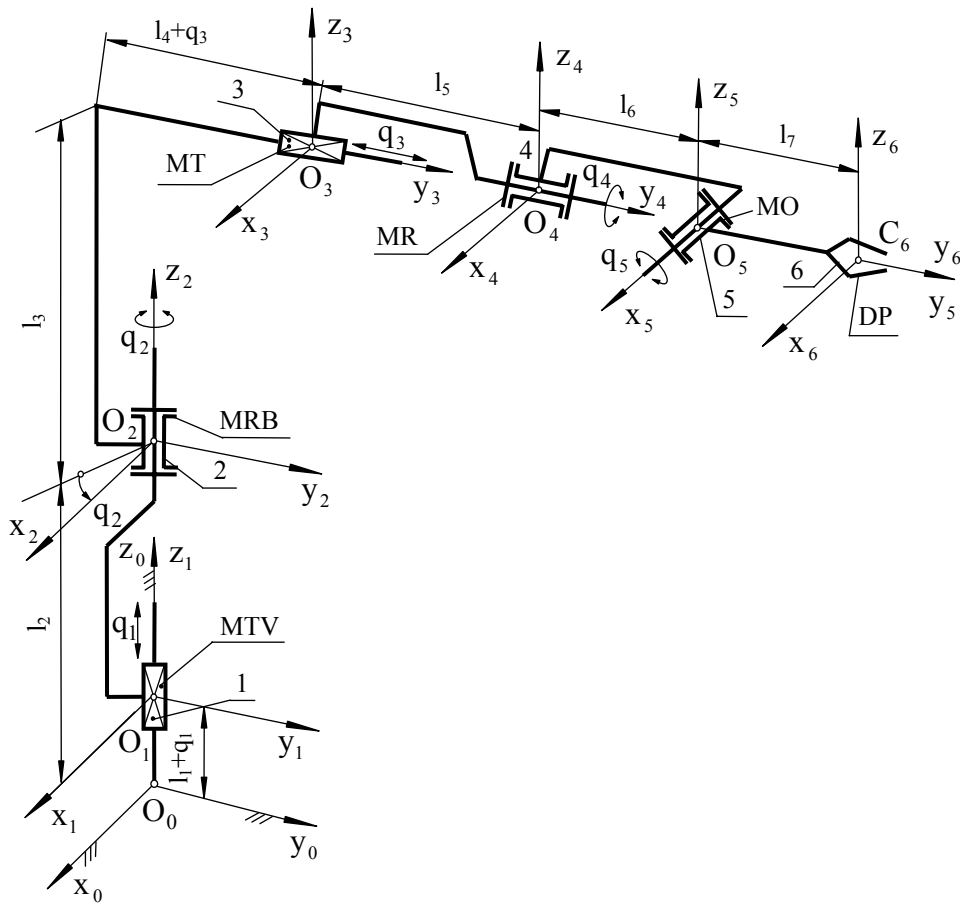


Fig.1. Structural Scheme of Kinematics for the Industrial Modular Serial Robot TRTRR

$$[T]_5^0(t) = \begin{bmatrix} cq_2cq_4 & -sq_2cq_5 + cq_2sq_4sq_5 & sq_2sq_5 + cq_2sq_4cq_5 & -(l_4 + l_5 + l_6 + q_3)sq_2 \\ sq_2cq_4 & cq_2cq_5 + sq_2sq_4sq_5 & -cq_2sq_5 + sq_2sq_4cq_5 & (l_4 + l_5 + l_6 + q_3)cq_2 \\ -sq_4 & cq_4sq_5 & cq_4cq_5 & l_1 + l_2 + l_3 + q_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}; \tag{6}$$

$$[T]_6^0(t) = \begin{bmatrix} cq_2cq_4 & -sq_2cq_5 + cq_2sq_4sq_5 & sq_2sq_5 + cq_2sq_4cq_5 & -(l_4 + l_5 + l_6 + q_3)sq_2 + l_7(-sq_2cq_5 + cq_2sq_4sq_5) \\ sq_2cq_4 & cq_2cq_5 + sq_2sq_4sq_5 & -cq_2sq_5 + sq_2sq_4cq_5 & (l_4 + l_5 + l_6 + q_3)cq_2 + l_7(cq_2cq_5 + sq_2sq_4sq_5) \\ -sq_4 & cq_4sq_5 & cq_4cq_5 & l_1 + l_2 + l_3 + q_1 + l_7cq_4sq_5 \\ 0 & 0 & 0 & 1 \end{bmatrix}. \tag{7}$$

Homogeneous transformation matrixes established following geometric modeling is used to determine the kinematics parameters $\bar{\omega}_i^i, \bar{v}_i^i, \bar{\varepsilon}_i^i, \bar{a}_i^i$. Using the relationship below is likely to determine the inverse of rotation matrixes:

$$[R]_{i-1}^i = [R_i^{i-1}]^{-1} = [R_i^{i-1}]^T. \tag{8}$$

Then, result:

$$[R]_0^1 = [I_3] = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}; [R]_1^2 = \begin{bmatrix} cq_2 & sq_2 & 0 \\ -sq_2 & cq_2 & 0 \\ 0 & 0 & 1 \end{bmatrix}; [R]_2^3 = [I_3] = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}; \tag{9}$$

$$\begin{aligned}
[R]_3^4 &= \begin{bmatrix} cq_4 & 0 & -sq_4 \\ 0 & 1 & 0 \\ sq_4 & 0 & cq_4 \end{bmatrix}; [R]_4^5 = \begin{bmatrix} 1 & 0 & 0 \\ 0 & cq_5 & sq_5 \\ 0 & -sq_5 & cq_5 \end{bmatrix}; \\
[R]_5^6 &= [I_3] = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}.
\end{aligned} \tag{10}$$

The unit vectors of kinematics axes (Fig. 1), are shown with matrix as follows:

$$\begin{aligned}
[\bar{k}]_1^1 &= \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}; [\bar{k}]_2^2 = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}; [\bar{j}]_3^3 = \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix}; \\
[\bar{j}]_4^4 &= \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix}; [\bar{i}]_5^5 = \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix}; [\bar{j}]_6^6 = \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix}.
\end{aligned} \tag{11}$$

Kinematics elements expressions, transposed with matrix, corresponding robot base, are the following:

$$[\bar{\omega}]_0^0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}; [\bar{v}]_0^0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}; [\bar{e}]_0^0 = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}; [\bar{a}]_0^0 = \begin{bmatrix} 0 \\ 0 \\ g \end{bmatrix}. \tag{12}$$

Operational rotation speeds are determined by inverse matrixes and with the kinematics parameters. So:

$$[\bar{\omega}]_1^1 = [R]_0^1 \cdot [\bar{\omega}]_0^0 = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}; \tag{13}$$

$$[\bar{\omega}]_2^2 = [R]_1^2 \cdot [\bar{\omega}]_1^1 + \dot{q}_2 \cdot [\bar{k}]_2^2 = \begin{bmatrix} cq_2 & sq_2 & 0 \\ -sq_2 & cq_2 & 0 \\ 0 & 0 & 1 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} + \dot{q}_2 \cdot \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ \dot{q}_2 \end{bmatrix}; \tag{14}$$

$$[\bar{\omega}]_3^3 = [R]_2^3 \cdot [\bar{\omega}]_2^2 = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ 0 \\ \dot{q}_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ \dot{q}_2 \end{bmatrix}; \tag{15}$$

$$\begin{aligned}
[\bar{\omega}]_4^4 &= [R]_3^4 \cdot [\bar{\omega}]_3^3 + \dot{q}_4 \cdot [\bar{j}]_4^4 = \begin{bmatrix} cq_4 & 0 & -sq_4 \\ 0 & 1 & 0 \\ sq_4 & 0 & cq_4 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ 0 \\ \dot{q}_2 \end{bmatrix} \\
&\cdot \begin{bmatrix} 0 \\ 0 \\ \dot{q}_2 \end{bmatrix} + \dot{q}_4 \cdot \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix} = \begin{bmatrix} -sq_4 \dot{q}_2 \\ \dot{q}_4 \\ cq_4 \dot{q}_2 \end{bmatrix};
\end{aligned} \tag{16}$$

$$[\bar{\omega}]_5^5 = [R]_4^5 \cdot [\bar{\omega}]_4^4 + \dot{q}_5 \cdot [\bar{i}]_5^5 = \begin{bmatrix} 1 & 0 & 0 \\ 0 & cq_5 & sq_5 \\ 0 & -sq_5 & cq_5 \end{bmatrix} \cdot \begin{bmatrix} -sq_4 \dot{q}_2 \\ \dot{q}_4 \\ cq_4 \dot{q}_2 \end{bmatrix} + \dot{q}_5 \cdot \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix}.$$

$$+ \dot{q}_5 \cdot \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} -sq_4 \dot{q}_2 + \dot{q}_5 \\ \dot{q}_4 cq_5 + \dot{q}_2 sq_5 cq_4 \\ -\dot{q}_4 sq_5 + \dot{q}_2 cq_5 cq_4 \end{bmatrix} \tag{17}$$

$$\begin{aligned}
[\bar{\omega}]_6^6 &= [R]_5^6 \cdot [\bar{\omega}]_5^5 = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \cdot \begin{bmatrix} -sq_4 \dot{q}_2 + \dot{q}_5 \\ \dot{q}_4 cq_5 + \dot{q}_2 sq_5 cq_4 \\ -\dot{q}_4 sq_5 + \dot{q}_2 cq_5 cq_4 \end{bmatrix} \\
&= \begin{bmatrix} -sq_4 \dot{q}_2 + \dot{q}_5 \\ \dot{q}_4 cq_5 + \dot{q}_2 sq_5 cq_4 \\ -\dot{q}_4 sq_5 + \dot{q}_2 cq_5 cq_4 \end{bmatrix}.
\end{aligned} \tag{18}$$

In accordance with [Ber93], [Neg01] and [Neg08], with opposite symmetric matrix 3x3 of the type $\{\bar{\omega} \times\}$, in which $\bar{\omega}$ represents the vector angular speed, it is of the form:

$$\{\bar{\omega} \times\} = \begin{bmatrix} 0 & -\omega_z & \omega_y \\ \omega_z & 0 & -\omega_x \\ -\omega_y & \omega_x & 0 \end{bmatrix}. \tag{19}$$

Vector products and double-vector products which still appear shall be expressed in accordance with the relationship (19). Linear speeds expressions transformed into operational matrix are the following:

$$\begin{aligned}
[\bar{v}]_1^1 &= [R]_0^1 \cdot \{[\bar{v}]_0^0 + [\bar{\omega}]_0^0 \times \bar{r}_1^0\} + \dot{q}_1 \cdot [\bar{k}]_1^1; \\
[\bar{v}]_1^1 &= \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \cdot \left\{ \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ 0 \\ l_1 + q_1 \end{bmatrix} \right\} + \dot{q}_1 \cdot \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ \dot{q}_1 \end{bmatrix};
\end{aligned} \tag{20}$$

$$\begin{aligned}
[\bar{v}]_2^2 &= [R]_1^2 \cdot \{[\bar{v}]_1^1 + \bar{\omega}_1^1 \times \bar{r}_2^1\}; \\
[\bar{v}]_2^2 &= \begin{bmatrix} cq_2 & sq_2 & 0 \\ -sq_2 & cq_2 & 0 \\ 0 & 0 & 1 \end{bmatrix} \cdot \left\{ \begin{bmatrix} 0 \\ 0 \\ \dot{q}_1 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ 0 \\ l_2 \end{bmatrix} \right\} = \begin{bmatrix} 0 \\ 0 \\ \dot{q}_1 \end{bmatrix};
\end{aligned} \tag{21}$$

$$\begin{aligned}
[\bar{v}]_3^3 &= [R]_2^3 \cdot \{[\bar{v}]_2^2 + \bar{\omega}_2^2 \times \bar{r}_3^2\} + \dot{q}_3 \cdot [\bar{j}]_3^3; \\
[\bar{v}]_3^3 &= \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \cdot \left\{ \begin{bmatrix} 0 \\ 0 \\ \dot{q}_1 \end{bmatrix} + \begin{bmatrix} 0 & -\dot{q}_2 & 0 \\ \dot{q}_2 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ l_4 + q_3 \\ l_3 \end{bmatrix} \right\} + \\
&+ \dot{q}_3 \cdot \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix} = \begin{bmatrix} -\dot{q}_2 (l_4 + q_3) \\ \dot{q}_3 \\ \dot{q}_1 \end{bmatrix};
\end{aligned} \tag{22}$$

$$\begin{aligned}
[\bar{v}]_4^4 &= [R]_3^4 \cdot \{\bar{v}_3^3 + \bar{\omega}_3^3 \times \bar{r}_4^3\}; \\
[\bar{v}]_4^4 &= \begin{bmatrix} cq_4 & 0 & -sq_4 \\ 0 & 1 & 0 \\ sq_4 & 0 & cq_4 \end{bmatrix} \cdot \left\{ \begin{bmatrix} -\dot{q}_2(l_4 + q_3) \\ \dot{q}_3 \\ \dot{q}_1 \end{bmatrix} + \begin{bmatrix} 0 & -\dot{q}_2 & 0 \\ \dot{q}_2 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ l_5 \\ 0 \end{bmatrix} \right\} = \begin{bmatrix} [-\dot{q}_2(l_4 + l_5 + q_3)]cq_4 - \dot{q}_1sq_4 \\ \dot{q}_3 \\ [-\dot{q}_2(l_4 + l_5 + q_3)]sq_4 + \dot{q}_1cq_4 \end{bmatrix};
\end{aligned} \tag{23}$$

$$\begin{aligned}
[\bar{v}]_5^5 &= [R]_4^5 \cdot \{\bar{v}_4^4 + \bar{\omega}_4^4 \times \bar{r}_5^4\}; \\
[\bar{v}]_5^5 &= \begin{bmatrix} 1 & 0 & 0 \\ 0 & cq_5 & sq_5 \\ 0 & -sq_5 & cq_5 \end{bmatrix} \cdot \left\{ \begin{bmatrix} [-\dot{q}_2(l_4 + l_5 + q_3)]cq_4 - \dot{q}_1sq_4 \\ \dot{q}_3 \\ [-\dot{q}_2(l_4 + l_5 + q_3)]sq_4 + \dot{q}_1cq_4 \end{bmatrix} + \begin{bmatrix} 0 & -\dot{q}_2cq_4 & \dot{q}_4 \\ \dot{q}_2cq_4 & 0 & \dot{q}_2sq_4 \\ -\dot{q}_4 & -\dot{q}_2sq_4 & 0 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ l_6 \\ 0 \end{bmatrix} \right\} = \\
&= \begin{bmatrix} [-\dot{q}_2(l_4 + l_5 + q_3)]cq_4 - \dot{q}_1sq_4 - \dot{q}_2l_6cq_4 \\ \dot{q}_3cq_5 + sq_5 \{[-\dot{q}_2(l_4 + l_5 + q_3)]sq_4 + \dot{q}_1cq_4 - \dot{q}_2l_6sq_4\} \\ -\dot{q}_3sq_5 + cq_5 \{[-\dot{q}_2(l_4 + l_5 + q_3)]sq_4 + \dot{q}_1cq_4 - \dot{q}_2l_6sq_4\} \end{bmatrix};
\end{aligned} \tag{24}$$

$$\begin{aligned}
[\bar{v}]_6^6 &= [R]_5^6 \cdot \{\bar{v}_5^5 + \bar{\omega}_5^5 \times \bar{r}_6^5\}; \\
[\bar{v}]_6^6 &= \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \cdot \left\{ \begin{bmatrix} [-\dot{q}_2(l_4 + l_5 + q_3)]cq_4 - \dot{q}_1sq_4 - \dot{q}_2l_6cq_4 \\ \dot{q}_3cq_5 + sq_5 \{[-\dot{q}_2(l_4 + l_5 + q_3)]sq_4 + \dot{q}_1cq_4 - \dot{q}_2l_6sq_4\} \\ -\dot{q}_3sq_5 + cq_5 \{[-\dot{q}_2(l_4 + l_5 + q_3)]sq_4 + \dot{q}_1cq_4 - \dot{q}_2l_6sq_4\} \end{bmatrix} + \right. \\
&+ \begin{bmatrix} 0 & \dot{q}_4sq_5 - \dot{q}_2cq_5cq_4 & \dot{q}_4cq_5 + \dot{q}_2sq_5cq_4 \\ -\dot{q}_4sq_5 + \dot{q}_2cq_5cq_4 & 0 & \dot{q}_2sq_4 - \dot{q}_5 \\ -\dot{q}_4cq_5 - \dot{q}_2sq_5cq_4 & -\dot{q}_2sq_4 + \dot{q}_5 & 0 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ l_7 \\ 0 \end{bmatrix} \left. \right\} = \\
&= \begin{bmatrix} [-\dot{q}_2(l_4 + l_5 + q_3)]cq_4 - \dot{q}_1sq_4 - \dot{q}_2l_6cq_4 + (\dot{q}_4sq_5 - \dot{q}_2cq_5cq_4)l_7 \\ \dot{q}_3cq_5 + sq_5 \{[-\dot{q}_2(l_4 + l_5 + q_3)]sq_4 + \dot{q}_1cq_4 - \dot{q}_2l_6sq_4\} \\ -\dot{q}_3sq_5 + cq_5 \{[-\dot{q}_2(l_4 + l_5 + q_3)]sq_4 + \dot{q}_1cq_4 - \dot{q}_2l_6sq_4\} + (-\dot{q}_2sq_4 + \dot{q}_5)l_7 \end{bmatrix}.
\end{aligned} \tag{25}$$

Similarly, can be expressed angular accelerations transformed into operational matrix. So:

$$[\bar{\varepsilon}]_1^1 = [R]_0^1 \cdot [\bar{\varepsilon}]_0^0; [\bar{\varepsilon}]_1^1 = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}; \tag{26}$$

$$[\bar{\varepsilon}]_3^3 = [R]_2^3 \cdot [\bar{\varepsilon}]_2^2; [\bar{\varepsilon}]_3^3 = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ 0 \\ \ddot{q}_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ \ddot{q}_2 \end{bmatrix}; \tag{28}$$

$$\begin{aligned}
[\bar{\varepsilon}]_2^2 &= [R]_1^2 \cdot [\bar{\varepsilon}]_1^1 + [R]_1^2 \cdot \bar{\omega}_1^2 \times \dot{q}_2 \cdot \bar{k}_2^2 + \ddot{q}_2 \cdot \bar{k}_2^2; [\bar{\varepsilon}]_2^2 = \begin{bmatrix} cq & sq & 0 \\ -sq & cq & 0 \\ 0 & 0 & 1 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} + \\
&+ \begin{bmatrix} cq & sq & 0 \\ -sq & cq & 0 \\ 0 & 0 & 1 \end{bmatrix} \cdot \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \cdot \dot{q}_2 \cdot \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} + \ddot{q}_2 \cdot \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ \ddot{q}_2 \end{bmatrix}; \\
[\bar{\varepsilon}]_4^4 &= [R]_3^4 \cdot [\bar{\varepsilon}]_3^3 + [R]_3^4 \cdot \bar{\omega}_3^4 \times \dot{q}_4 \cdot \bar{J}_4^4 + \ddot{q}_4 \cdot \bar{J}_4^4; [\bar{\varepsilon}]_4^4 = \begin{bmatrix} cq & 0 & -sq \\ 0 & 1 & 0 \\ sq & 0 & cq \end{bmatrix} \cdot \begin{bmatrix} 0 \\ 0 \\ \ddot{q}_2 \end{bmatrix} + \\
&+ \begin{bmatrix} cq & 0 & -sq \\ 0 & 1 & 0 \\ sq & 0 & cq \end{bmatrix} \cdot \begin{bmatrix} 0 & -\dot{q}_2 & 0 \\ \dot{q}_2 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ \dot{q}_4 \\ 0 \end{bmatrix} + \ddot{q}_4 \cdot \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} -\dot{q}_2sq - \dot{q}_2\dot{q}_4cq \\ \ddot{q}_4 \\ \dot{q}_2cq - \dot{q}_2\dot{q}_4sq \end{bmatrix};
\end{aligned} \tag{29}$$

(27)

$$\begin{aligned}
[\bar{\varepsilon}]_5^5 &= [\mathbf{R}]_4^5 \cdot [\bar{\varepsilon}]_4^4 + \{[\mathbf{R}]_4^5 \cdot \bar{\omega}_4^4 \times \dot{q}_5 \cdot \bar{i}_5^5 + \ddot{q}_5 \cdot \bar{i}_5^5\}; \\
[\bar{\varepsilon}]_5^5 &= \begin{bmatrix} 1 & 0 & 0 \\ 0 & cq_5 & sq_5 \\ 0 & -sq_5 & cq_5 \end{bmatrix} \cdot \begin{bmatrix} -\ddot{q}_2sq_4 - \dot{q}_2\dot{q}_4cq_4 \\ \ddot{q}_4 \\ \ddot{q}_2cq_4 - \dot{q}_2\dot{q}_4sq_4 \end{bmatrix} + \left\{ \begin{bmatrix} 1 & 0 & 0 \\ 0 & cq_5 & sq_5 \\ 0 & -sq_5 & cq_5 \end{bmatrix} \cdot \begin{bmatrix} 0 & -\dot{q}_2cq_4 & \dot{q}_4 \\ \dot{q}_2cq_4 & 0 & \dot{q}_2sq_4 \\ -\dot{q}_4 & -\dot{q}_2sq_4 & 0 \end{bmatrix} \right. \\
&\quad \cdot \begin{bmatrix} \dot{q}_5 \\ 0 \\ 0 \end{bmatrix} + \left. \begin{bmatrix} \ddot{q}_5 \\ 0 \\ 0 \end{bmatrix} \right\} = \begin{bmatrix} -\ddot{q}_2sq_4 - \dot{q}_2\dot{q}_4cq_4 + \ddot{q}_5 \\ \ddot{q}_4cq_5 + sq_5(\ddot{q}_2cq_4 - \dot{q}_2\dot{q}_4sq_4) + \dot{q}_5(\dot{q}_2cq_5cq_4 - \dot{q}_4sq_5) \\ -\ddot{q}_4sq_5 + cq_5(\ddot{q}_2cq_4 - \dot{q}_2\dot{q}_4sq_4) + \dot{q}_5(-\dot{q}_2sq_5cq_4 - \dot{q}_4cq_5) \end{bmatrix}; \tag{30}
\end{aligned}$$

$$\begin{aligned}
[\bar{\varepsilon}]_6^6 &= [\mathbf{R}]_5^6 \cdot [\bar{\varepsilon}]_5^5; \\
[\bar{\varepsilon}]_6^6 &= \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \cdot \begin{bmatrix} -\ddot{q}_2sq_4 - \dot{q}_2\dot{q}_4cq_4 + \ddot{q}_5 \\ \ddot{q}_4cq_5 + sq_5(\ddot{q}_2cq_4 - \dot{q}_2\dot{q}_4sq_4) + \dot{q}_5(\dot{q}_2cq_5cq_4 - \dot{q}_4sq_5) \\ -\ddot{q}_4sq_5 + cq_5(\ddot{q}_2cq_4 - \dot{q}_2\dot{q}_4sq_4) + \dot{q}_5(-\dot{q}_2sq_5cq_4 - \dot{q}_4cq_5) \end{bmatrix} = \\
&= \begin{bmatrix} -\ddot{q}_2sq_4 - \dot{q}_2\dot{q}_4cq_4 + \ddot{q}_5 \\ \ddot{q}_4cq_5 + sq_5(\ddot{q}_2cq_4 - \dot{q}_2\dot{q}_4sq_4) + \dot{q}_5(\dot{q}_2cq_5cq_4 - \dot{q}_4sq_5) \\ -\ddot{q}_4sq_5 + cq_5(\ddot{q}_2cq_4 - \dot{q}_2\dot{q}_4sq_4) + \dot{q}_5(-\dot{q}_2sq_5cq_4 - \dot{q}_4cq_5) \end{bmatrix}. \tag{31}
\end{aligned}$$

In accordance with the relationship [Isp04], expressions of operational linear acceleration are as follows:

$$\begin{aligned}
[\bar{a}]_1^1 &= [\mathbf{R}]_0^1 \cdot \{ \bar{a}_0^0 + \bar{\varepsilon}_0^0 \times \bar{r}_1^0 + \bar{\omega}_0^0 \times (\bar{\omega}_0^0 \times \bar{r}_1^0) \} + \{ 2\bar{\omega}_1^1 \times \dot{q}_1 \cdot \bar{k}_1^1 + \ddot{q}_1 \cdot \bar{k}_1^1 \}; \\
[\bar{a}]_1^1 &= \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \cdot \left\{ \begin{bmatrix} 0 \\ 0 \\ g \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ 0 \\ l_1 + q_1 \end{bmatrix} + \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ 0 \\ l_1 + q_1 \end{bmatrix} \right\} + \\
&\quad \cdot \left\{ \begin{bmatrix} 0 \\ 0 \\ \ddot{q}_1 + g \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ 0 \\ l_2 \end{bmatrix} + \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ 0 \\ l_2 \end{bmatrix} \right\} = \begin{bmatrix} 0 \\ 0 \\ \ddot{q}_1 + g \end{bmatrix}; \tag{32} \\
&\quad + \left\{ 2 \cdot \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \cdot \dot{q}_1 \cdot \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} + \dot{q}_1 \cdot \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \right\} = \begin{bmatrix} 0 \\ 0 \\ \ddot{q}_1 + g \end{bmatrix}; \tag{33}
\end{aligned}$$

$$\begin{aligned}
[\bar{a}]_3^3 &= [\mathbf{R}]_2^3 \cdot \{ \bar{a}_2^2 + \bar{\varepsilon}_2^2 \times \bar{r}_3^2 + \bar{\omega}_2^2 \times (\bar{\omega}_2^2 \times \bar{r}_3^2) \} + \{ 2\bar{\omega}_3^3 \times \dot{q}_3 \cdot \bar{j}_3^3 + \ddot{q}_3 \cdot \bar{j}_3^3 \}; \\
[\bar{a}]_3^3 &= \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \cdot \left\{ \begin{bmatrix} 0 \\ 0 \\ \ddot{q}_1 + g \end{bmatrix} + \begin{bmatrix} 0 & -\ddot{q}_2 & 0 \\ \ddot{q}_2 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ 0 \\ l_3 \end{bmatrix} + \begin{bmatrix} 0 & -\dot{q}_2 & 0 \\ \dot{q}_2 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \cdot \begin{bmatrix} 0 & -\dot{q}_2 & 0 \\ \dot{q}_2 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \cdot \begin{bmatrix} 0 & -\dot{q}_2 & 0 \\ \dot{q}_2 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \right. \\
&\quad \cdot \begin{bmatrix} 0 \\ l_4 + q_3 \\ l_3 \end{bmatrix} \left. \right\} + \left\{ 2 \cdot \begin{bmatrix} 0 & -\dot{q}_2 & 0 \\ \dot{q}_2 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \right\} = \begin{bmatrix} -\ddot{q}_2(l_4 + q_3) - 2\dot{q}_2\dot{q}_3 \\ -\dot{q}_2^2(l_4 + q_3) + \ddot{q}_3 \\ \ddot{q}_1 + g \end{bmatrix}; \tag{34}
\end{aligned}$$

$$\begin{aligned}
[\bar{\mathbf{a}}]_4^4 &= [\mathbf{R}]_3^4 \cdot \left\{ \bar{\mathbf{a}}_3^3 + \bar{\varepsilon}_3^3 \times \bar{\mathbf{r}}_4^3 + \bar{\omega}_3^3 \times (\bar{\omega}_3^3 \times \bar{\mathbf{r}}_4^3) \right\}; \\
[\bar{\mathbf{a}}]_4^4 &= \begin{bmatrix} \text{cq}_4 & 0 & -\text{sq}_4 \\ 0 & 1 & 0 \\ \text{sq}_4 & 0 & \text{cq}_4 \end{bmatrix} \cdot \left\{ \begin{bmatrix} -\ddot{q}_2(l_4 + q_3) - 2\dot{q}_2\dot{q}_3 \\ -\dot{q}_2^2(l_4 + q_3) + \ddot{q}_3 \\ \ddot{q}_1 + g \end{bmatrix} + \begin{bmatrix} 0 & -\ddot{q}_2 & 0 \\ \ddot{q}_2 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ l_5 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 & -\dot{q}_2 & 0 \\ \dot{q}_2 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ l_5 \\ 0 \end{bmatrix} \right\} \\
&= \begin{bmatrix} 0 & -\dot{q}_2 & 0 \\ \dot{q}_2 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ l_5 \\ 0 \end{bmatrix} = \begin{bmatrix} \text{cq}_4[-\ddot{q}_2(l_4 + l_5 + q_3) - 2\dot{q}_2\dot{q}_3] - \text{sq}_4(\ddot{q}_1 + g) \\ -\dot{q}_2^2(l_4 + l_5 + q_3) + \ddot{q}_3 \\ \text{sq}_4[-\ddot{q}_2(l_4 + l_5 + q_3) - 2\dot{q}_2\dot{q}_3] + \text{cq}_4(\ddot{q}_1 + g) \end{bmatrix}; \tag{35}
\end{aligned}$$

$$\begin{aligned}
[\bar{\mathbf{a}}]_5^5 &= [\mathbf{R}]_4^5 \cdot \left\{ \bar{\mathbf{a}}_4^4 + \bar{\varepsilon}_4^4 \times \bar{\mathbf{r}}_5^4 + \bar{\omega}_4^4 \times (\bar{\omega}_4^4 \times \bar{\mathbf{r}}_5^4) \right\}; \\
[\bar{\mathbf{a}}]_5^5 &= \begin{bmatrix} 1 & 0 & 0 \\ 0 & \text{cq}_5 & \text{sq}_5 \\ 0 & -\text{sq}_5 & \text{cq}_5 \end{bmatrix} \cdot \left\{ \begin{bmatrix} \text{cq}_4[-\ddot{q}_2(l_4 + l_5 + q_3) - 2\dot{q}_2\dot{q}_3] - \text{sq}_4(\ddot{q}_1 + g) \\ -\dot{q}_2^2(l_4 + l_5 + q_3) + \ddot{q}_3 \\ \text{sq}_4[-\ddot{q}_2(l_4 + l_5 + q_3) - 2\dot{q}_2\dot{q}_3] + \text{cq}_4(\ddot{q}_1 + g) \end{bmatrix} + \right. \\
&+ \begin{bmatrix} 0 & -\ddot{q}_2\text{cq}_4 + \dot{q}_2\dot{q}_4\text{sq}_4 & \ddot{q}_4 \\ \ddot{q}_2\text{cq}_4 - \dot{q}_2\dot{q}_4\text{sq}_4 & 0 & \ddot{q}_2\text{sq}_4 + \dot{q}_2\dot{q}_4\text{cq}_4 \\ -\ddot{q}_4 & -\ddot{q}_2\text{sq}_4 - \dot{q}_2\dot{q}_4\text{cq}_4 & 0 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ l_6 \\ 0 \end{bmatrix} + \\
&+ \begin{bmatrix} 0 & -\dot{q}_2\text{cq}_4 & \dot{q}_4 \\ \dot{q}_2\text{cq}_4 & 0 & \dot{q}_2\text{sq}_4 \\ -\dot{q}_4 & -\dot{q}_2\text{sq}_4 & 0 \end{bmatrix} \cdot \begin{bmatrix} 0 & -\dot{q}_2\text{cq}_4 & \dot{q}_4 \\ \dot{q}_2\text{cq}_4 & 0 & \dot{q}_2\text{sq}_4 \\ -\dot{q}_4 & -\dot{q}_2\text{sq}_4 & 0 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ l_6 \\ 0 \end{bmatrix} \left. \right\} = \\
&= \begin{bmatrix} \text{cq}_4[-\ddot{q}_2(l_4 + l_5 + q_3) - 2\dot{q}_2\dot{q}_3] - \text{sq}_4(\ddot{q}_1 + g) + (\ddot{q}_2\text{cq}_4 + \dot{q}_2\dot{q}_4\text{sq}_4)l_6 - \dot{q}_2\dot{q}_4l_6\text{sq}_4 \\ \text{cq}_5[-\dot{q}_2^2(l_4 + l_5 + q_3) + \ddot{q}_3 + (-c^2q_4\dot{q}_2^2 - s^2q_4\dot{q}_2^2)l_6] + \text{sq}_5\{\text{sq}_4[-\ddot{q}_2(l_4 + l_5 + q_3) - 2\dot{q}_2\dot{q}_3] + \text{cq}_4(\ddot{q}_1 + g) + (-\ddot{q}_2\text{sq}_4 - \dot{q}_2\dot{q}_4\text{cq}_4)l_6 + \dot{q}_2\dot{q}_4l_6\text{cq}_4\} \\ -\text{sq}_5[-\dot{q}_2^2(l_4 + l_5 + q_3) + \ddot{q}_3 + (-c^2q_4\dot{q}_2^2 - s^2q_4\dot{q}_2^2)l_6] + \text{cq}_5\{\text{sq}_4[-\ddot{q}_2(l_4 + l_5 + q_3) - 2\dot{q}_2\dot{q}_3] + \text{cq}_4(\ddot{q}_1 + g) + (-\ddot{q}_2\text{sq}_4 - \dot{q}_2\dot{q}_4\text{cq}_4)l_6 + \dot{q}_2\dot{q}_4l_6\text{cq}_4\} \end{bmatrix}; \tag{36}
\end{aligned}$$

$$\begin{aligned}
[\bar{\mathbf{a}}]_6^6 &= [\mathbf{R}]_5^6 \cdot \left\{ \bar{\mathbf{a}}_5^5 + \bar{\varepsilon}_5^5 \times \bar{\mathbf{r}}_6^5 + \bar{\omega}_5^5 \times (\bar{\omega}_5^5 \times \bar{\mathbf{r}}_6^5) \right\}; \\
[\bar{\mathbf{a}}]_6^6 &= \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \cdot \left\{ \begin{bmatrix} \text{cq}_4[-\ddot{q}_2(l_4 + l_5 + q_3) - 2\dot{q}_2\dot{q}_3] - \text{sq}_4(\ddot{q}_1 + g) + \\ + (\ddot{q}_2\text{cq}_4 + \dot{q}_2\dot{q}_4\text{sq}_4)l_6 - \dot{q}_2\dot{q}_4l_6\text{sq}_4 \\ \text{cq}_5[-\dot{q}_2^2(l_4 + l_5 + q_3) + \ddot{q}_3 + (-c^2q_4\dot{q}_2^2 - s^2q_4\dot{q}_2^2)l_6] + \\ + \text{sq}_5\{\text{sq}_4[-\ddot{q}_2(l_4 + l_5 + q_3) - 2\dot{q}_2\dot{q}_3] + \text{cq}_4(\ddot{q}_1 + g) + \\ + (-\ddot{q}_2\text{sq}_4 - \dot{q}_2\dot{q}_4\text{cq}_4)l_6 + \dot{q}_2\dot{q}_4l_6\text{cq}_4\} \\ -\text{sq}_5[-\dot{q}_2^2(l_4 + l_5 + q_3) + \ddot{q}_3 + (-c^2q_4\dot{q}_2^2 - s^2q_4\dot{q}_2^2)l_6] + \\ + \text{cq}_5\{\text{sq}_4[-\ddot{q}_2(l_4 + l_5 + q_3) - 2\dot{q}_2\dot{q}_3] + \text{cq}_4(\ddot{q}_1 + g) + \\ + (-\ddot{q}_2\text{sq}_4 - \dot{q}_2\dot{q}_4\text{cq}_4)l_6 + \dot{q}_2\dot{q}_4l_6\text{cq}_4\} \end{bmatrix} + \right.
\end{aligned}$$

$$\begin{aligned}
& \left[\begin{array}{ccc|ccc}
0 & \ddot{q}_4 s q_5 - & \ddot{q}_4 c q_5 + \\
& - c q_5 (\ddot{q}_2 c q_4 - \dot{q}_2 \dot{q}_4 s q_4) - & + s q_5 (\ddot{q}_2 c q_4 - \dot{q}_2 \dot{q}_4 s q_4) + \\
& - \dot{q}_5 (-\dot{q}_2 s q_5 c q_4 - \dot{q}_4 c q_5) & + \dot{q}_5 (\dot{q}_2 c q_5 c q_4 - \dot{q}_4 s q_5) \\
\hline
- \ddot{q}_4 s q_5 + & & \\
+ c q_5 (\ddot{q}_2 c q_4 - \dot{q}_2 \dot{q}_4 s q_4) + & 0 & \ddot{q}_2 s q_4 + \dot{q}_2 \dot{q}_4 c q_4 - \ddot{q}_5 \\
+ \dot{q}_5 (-\dot{q}_2 s q_5 c q_4 - \dot{q}_4 c q_5) & & \\
\hline
- \ddot{q}_4 c q_5 - & & \\
- s q_5 (\ddot{q}_2 c q_4 - \dot{q}_2 \dot{q}_4 s q_4) - & - \ddot{q}_2 s q_4 - \dot{q}_2 \dot{q}_4 c q_4 + \ddot{q}_5 & 0 \\
- \dot{q}_5 (\dot{q}_2 c q_5 c q_4 - \dot{q}_4 s q_5) & &
\end{array} \right] \cdot \begin{bmatrix} 0 \\ 1_7 \\ 0 \end{bmatrix} + \\
& + \left[\begin{array}{ccc}
0 & \dot{q}_4 s q_5 - \dot{q}_2 c q_5 c q_4 & \dot{q}_4 c q_5 + \dot{q}_2 s q_5 c q_4 \\
- \dot{q}_4 s q_5 + \dot{q}_2 c q_5 c q_4 & 0 & \dot{q}_2 s q_4 - \dot{q}_5 \\
- \dot{q}_4 c q_5 - \dot{q}_2 s q_5 c q_4 & - \dot{q}_2 s q_4 + \dot{q}_5 & 0
\end{array} \right] \cdot \\
& \cdot \left[\begin{array}{ccc}
0 & \dot{q}_4 s q_5 - \dot{q}_2 c q_5 c q_4 & \dot{q}_4 c q_5 + \dot{q}_2 s q_5 c q_4 \\
- \dot{q}_4 s q_5 + \dot{q}_2 c q_5 c q_4 & 0 & \dot{q}_2 s q_4 - \dot{q}_5 \\
- \dot{q}_4 c q_5 - \dot{q}_2 s q_5 c q_4 & - \dot{q}_2 s q_4 + \dot{q}_5 & 0
\end{array} \right] \cdot \begin{bmatrix} 0 \\ 1_7 \\ 0 \end{bmatrix} = \\
& = \left[\begin{array}{l}
c q_4 [-\ddot{q}_2 (l_4 + l_5 + q_3) - 2\dot{q}_2 \dot{q}_3] - s q_4 (\ddot{q}_1 + g) + (\ddot{q}_2 c q_4 + \dot{q}_2 \dot{q}_4 s q_4) l_6 - \dot{q}_2 \dot{q}_4 l_6 s q_4 + \\
+ [\ddot{q}_4 s q_5 - c q_5 (\ddot{q}_2 c q_4 - \dot{q}_2 \dot{q}_4 s q_4) - \dot{q}_5 (-\dot{q}_2 s q_5 c q_4 - \dot{q}_4 c q_5)] l_7 + \\
+ (\dot{q}_4 c q_5 + \dot{q}_2 s q_5 c q_4) \cdot (-\dot{q}_2 s q_4 + \dot{q}_5) l_7 \\
\hline
c q_5 [-\dot{q}_2^2 (l_4 + l_5 + q_3) + \ddot{q}_3 + (-c^2 q_4 \dot{q}_2^2 - s^2 q_4 \dot{q}_2^2) l_6] + \\
+ s q_5 \{s q_4 [-\ddot{q}_2 (l_4 + l_5 + q_3) - 2\dot{q}_2 \dot{q}_3] + c q_4 (\ddot{q}_1 + g) + \\
+ (-\ddot{q}_2 s q_4 - \dot{q}_2 \dot{q}_4 c q_4) l_6 + \dot{q}_2 \dot{q}_4 l_6 c q_4 \} + [(-\dot{q}_2 c q_4 c q_5 + \dot{q}_4 s q_5) \cdot \\
\cdot (\dot{q}_2 c q_4 c q_5 - \dot{q}_4 s q_5) + (\dot{q}_2 s q_4 - \dot{q}_5) \cdot (-\dot{q}_2 s q_4 + \dot{q}_5) l_7] \\
\hline
- s q_5 [-\dot{q}_2^2 (l_4 + l_5 + q_3) + \ddot{q}_3 + (-c^2 q_4 \dot{q}_2^2 - s^2 q_4 \dot{q}_2^2) l_6] + \\
+ c q_5 \{s q_4 [-\ddot{q}_2 (l_4 + l_5 + q_3) - 2\dot{q}_2 \dot{q}_3] + c q_4 (\ddot{q}_1 + g) + \\
+ (-\ddot{q}_2 s q_4 - \dot{q}_2 \dot{q}_4 c q_4) l_6 + \dot{q}_2 \dot{q}_4 l_6 c q_4 \} + (-\ddot{q}_2 s q_4 - \dot{q}_4 \dot{q}_2 c q_4 + \ddot{q}_5) l_7 + \\
+ [(-\dot{q}_2 c q_4 s q_5 - \dot{q}_4 c q_5) \cdot (-\dot{q}_2 c q_4 c q_5 + \dot{q}_4 s q_5)] l_7
\end{array} \right] \quad (37)
\end{aligned}$$

Kinematics operational parameters in the system $O_{6x_6y_6z_6}$ may be written, in accordance with (ISP04), following form:

$$\left[\begin{array}{c} \dot{X} \end{array} \right]^6 = \left[\begin{array}{c} [-\dot{q}_2 (l_4 + l_5 + q_3)] c q_4 - \dot{q}_1 s q_4 - \dot{q}_2 l_6 c q_4 + (\dot{q}_4 s q_5 - \dot{q}_2 c q_5 c q_4) l_7 \\ \dot{q}_3 c q_5 + s q_5 \{[-\dot{q}_2 (l_4 + l_5 + q_3)] s q_4 + \dot{q}_1 c q_4 - \dot{q}_2 l_6 s q_4 \} \\ - \dot{q}_3 s q_5 + c q_5 \{[-\dot{q}_2 (l_4 + l_5 + q_3)] s q_4 + \dot{q}_1 c q_4 - \dot{q}_2 l_6 s q_4 \} + (-\dot{q}_2 s q_4 + \dot{q}_5) l_7 \\ - s q_4 \dot{q}_2 + \dot{q}_5 \\ \dot{q}_4 c q_5 + \dot{q}_2 s q_5 c q_4 \\ - \dot{q}_4 s q_5 + \dot{q}_2 c q_5 c q_4 \end{array} \right], \quad (38)$$

$$\begin{aligned}
\left[\ddot{\bar{X}} \right]_6^6 = & \left[\begin{array}{l}
cq_4[-\ddot{q}_2(l_4 + l_5 + q_3) - 2\dot{q}_2\dot{q}_3] - sq_4(\ddot{q}_1 + g) + (\ddot{q}_2cq_4 + \dot{q}_2\dot{q}_4sq_4)l_6 - \dot{q}_2\dot{q}_4l_6sq_4 + \\
+ [\dot{q}_4sq_5 - cq_5(\ddot{q}_2cq_4 - \dot{q}_2\dot{q}_4sq_4) - \dot{q}_5(-\dot{q}_2sq_5cq_4 - \dot{q}_4cq_5)]l_7 + \\
+ (\dot{q}_4cq_5 + \dot{q}_2sq_5cq_4) \cdot (-\dot{q}_2sq_4 + \dot{q}_5)l_7 \\
\hline
cq_5[-\dot{q}_2^2(l_4 + l_5 + q_3) + \ddot{q}_3 + (-c^2q_4\dot{q}_2^2 - s^2q_4\dot{q}_2^2)l_6] + \\
+ sq_5\{sq_4[-\ddot{q}_2(l_4 + l_5 + q_3) - 2\dot{q}_2\dot{q}_3] + cq_4(\ddot{q}_1 + g) + \\
+ (-\dot{q}_2sq_4 - \dot{q}_2\dot{q}_4cq_4)l_6 + \dot{q}_2\dot{q}_4l_6cq_4\} + [(-\dot{q}_2cq_4cq_5 + \dot{q}_4sq_5) \cdot \\
\cdot (\dot{q}_2cq_4cq_5 - \dot{q}_4sq_5) + (\dot{q}_2sq_4 - \dot{q}_5) \cdot (-\dot{q}_2sq_4 + \dot{q}_5)l_7] \\
\hline
-sq_5[-\dot{q}_2^2(l_4 + l_5 + q_3) + \ddot{q}_3 + (-c^2q_4\dot{q}_2^2 - s^2q_4\dot{q}_2^2)l_6] + \\
+ cq_5\{sq_4[-\ddot{q}_2(l_4 + l_5 + q_3) - 2\dot{q}_2\dot{q}_3] + cq_4(\ddot{q}_1 + g) + \\
+ (-\dot{q}_2sq_4 - \dot{q}_2\dot{q}_4cq_4)l_6 + \dot{q}_2\dot{q}_4l_6cq_4\} + (-\dot{q}_2sq_4 - \dot{q}_4\dot{q}_2cq_4 + \ddot{q}_5)l_7 + \\
+ [(-\dot{q}_2cq_4sq_5 - \dot{q}_4cq_5) \cdot (-\dot{q}_2cq_4cq_5 + \dot{q}_4sq_5)]l_7 \\
\hline
-\ddot{q}_2sq_4 - \dot{q}_2\dot{q}_4cq_4 + \ddot{q}_5 \\
\hline
\frac{\ddot{q}_4cq_5 + sq_5(\ddot{q}_2cq_4 - \dot{q}_2\dot{q}_4sq_4) + \dot{q}_5(\dot{q}_2cq_5cq_4 - \dot{q}_4sq_5)}{-\dot{q}_4sq_5 + cq_5(\ddot{q}_2cq_4 - \dot{q}_2\dot{q}_4sq_4) + \dot{q}_5(-\dot{q}_2sq_5cq_4 - \dot{q}_4cq_5)}
\end{array} \right] \quad (39)
\end{aligned}$$

Using relations of processing, the kinematics parameters can be determined of the fixed system operational $O_{0x_0y_0z_0}$ at the base robot. Those relations are:

$$\left[\bar{v} \right]_6^0 = [R]_6^0 \cdot \left[\bar{v} \right]_6^6, \quad (40)$$

$$\begin{aligned}
\left[\bar{v} \right]_6^0 = & \left[\begin{array}{ccc}
cq_2cq_4 & -sq_2cq_5 + cq_2sq_4sq_5 & sq_2sq_5 + cq_2sq_4cq_5 \\
sq_2cq_4 & cq_2cq_5 + sq_2sq_4sq_5 & -cq_2sq_5 + sq_2sq_4cq_5 \\
-sq_4 & cq_4sq_5 & cq_4cq_5
\end{array} \right] \cdot \\
& \left[\begin{array}{l}
[-\dot{q}_2(l_4 + l_5 + q_3)]cq_4 - \dot{q}_1sq_4 - \dot{q}_2l_6cq_4 + (\dot{q}_4sq_5 - \dot{q}_2cq_5cq_4)l_7 \\
\dot{q}_3cq_5 + sq_5\{-\dot{q}_2(l_4 + l_5 + q_3)\}sq_4 + \dot{q}_1cq_4 - \dot{q}_2l_6sq_4\} \\
-\dot{q}_3sq_5 + cq_5\{-\dot{q}_2(l_4 + l_5 + q_3)\}sq_4 + \dot{q}_1cq_4 - \dot{q}_2l_6sq_4\} + (-\dot{q}_2sq_4 + \dot{q}_5)l_7
\end{array} \right] = \\
& \left[\begin{array}{l}
\dot{q}_4l_7cq_2cq_4sq_5 - \dot{q}_3sq_2 - \dot{q}_2l_7sq_2sq_4sq_5 + \dot{q}_5l_7sq_2sq_5 - \dot{q}_2q_3cq_2 - l_4\dot{q}_2cq_2 - l_5\dot{q}_2cq_2 - \\
-l_6\dot{q}_2cq_2 + \dot{q}_5l_7cq_2sq_4cq_5 - \dot{q}_2l_7cq_2cq_5 \\
\dot{q}_3cq_2 - \dot{q}_5l_7cq_2sq_5 - \dot{q}_2q_3sq_2 - l_4\dot{q}_2sq_2 - l_5\dot{q}_2sq_2 - l_6\dot{q}_2sq_2 + \dot{q}_4l_7sq_2cq_4sq_5 + \\
+ \dot{q}_2l_7cq_2sq_4sq_5 + \dot{q}_5l_7sq_2sq_4cq_5 - \dot{q}_2l_7sq_2cq_5 \\
\dot{q}_1 - \dot{q}_4l_7sq_4sq_5 + \dot{q}_5l_7cq_5cq_4
\end{array} \right]; \quad (41)
\end{aligned}$$

$$\left[\bar{\omega} \right]_6^0 = [R]_6^0 \cdot \left[\bar{\omega} \right]_6^6, \quad \left[\bar{\omega} \right]_6^0 = \left[\begin{array}{l}
\dot{q}_5cq_2cq_4 - \dot{q}_4sq_2 \\
\dot{q}_5sq_2cq_4 + \dot{q}_4cq_2 \\
\dot{q}_2 - \dot{q}_5sq_4
\end{array} \right]; \quad (42)$$

$$\begin{aligned}
[\bar{a}]_6^0 &= [R]_6^0 \cdot [\bar{a}]_6^6, \\
[\bar{a}]_6^0 &= \begin{bmatrix}
-\ddot{q}_3 s q_2 - \ddot{q}_2 l_7 s q_2 s q_5 s q_4 - 2\dot{q}_2 \dot{q}_4 l_7 s q_2 s q_5 c q_4 + \ddot{q}_5 l_7 c q_2 s q_4 c q_5 + \ddot{q}_5 l_7 s q_2 s q_5 + \\
+ 2\dot{q}_2 \dot{q}_5 l_7 c q_2 s q_5 + \dot{q}_5^2 l_7 s q_2 c q_5 + \dot{q}_2^2 l_5 s q_2 + q_3 \dot{q}_2^2 s q_2 + \dot{q}_2^2 l_4 s q_2 - \\
-\ddot{q}_2 l_6 c q_2 - \ddot{q}_2 l_7 c q_2 c q_5 - q_3 \ddot{q}_2 c q_2 - \ddot{q}_2 l_4 c q_2 - \dot{q}_4^2 l_7 c q_2 s q_4 s q_5 - \\
-\dot{q}_2^2 l_7 c q_2 s q_4 s q_5 - 2\dot{q}_2 \dot{q}_3 c q_2 - \ddot{q}_5 l_5 c q_2 + \dot{q}_2^2 l_7 s q_2 c q_5 + \dot{q}_2^2 l_6 s q_2 - \\
-\dot{q}_2 \dot{q}_5 l_7 s q_2 c q_5 s q_4 + \ddot{q}_4 l_7 c q_2 c q_4 s q_5 + 2\dot{q}_4 \dot{q}_5 l_7 c q_2 c q_4 c q_5 - \dot{q}_5^2 l_7 c q_2 s q_4 s q_5 \\
-\ddot{q}_2 l_6 s q_2 - \dot{q}_2^2 l_7 c q_2 c q_5 - q_3 \ddot{q}_2 s q_2 - \dot{q}_4^2 l_7 s q_2 s q_4 s q_5 + 2\dot{q}_2 \dot{q}_5 l_7 s q_2 s q_5 - \\
-\dot{q}_2^2 l_7 s q_2 s q_4 s q_5 - \dot{q}_2^2 l_6 c q_2 - 2\dot{q}_2 \dot{q}_3 s q_2 - \ddot{q}_2 l_4 s q_2 - \dot{q}_2^2 l_4 c q_2 - \ddot{q}_5 l_5 s q_2 - \\
-\ddot{q}_2 l_7 s q_2 c q_5 - \dot{q}_2^2 l_5 c q_2 - q_3 \dot{q}_2^2 c q_2 + \ddot{q}_3 c q_2 - \dot{q}_2^2 l_7 c q_2 c q_5 - \ddot{q}_5 l_7 c q_2 s q_5 + \\
+ \ddot{q}_4 l_7 s q_2 c q_4 s q_5 + 2\dot{q}_4 \dot{q}_5 l_7 s q_2 c q_4 c q_5 + 2\dot{q}_2 \dot{q}_5 l_7 c q_2 c q_5 s q_4 - \dot{q}_5^2 l_7 s q_2 s q_4 s q_5 + \\
+ \ddot{q}_2 l_7 c q_2 s q_5 s q_4 + 2\dot{q}_2 \dot{q}_4 l_7 c q_2 s q_5 c q_4 + \ddot{q}_5 l_7 s q_2 s q_4 c q_5 \\
\hline
\ddot{q}_1 + g - \dot{q}_4^2 l_7 c q_4 s q_5 - \ddot{q}_4 l_7 s q_4 s q_5 - \dot{q}_5^2 l_7 c q_4 s q_5 - 2\dot{q}_4 \dot{q}_5 l_7 s q_4 c q_5 + \ddot{q}_5 l_7 c q_4 c q_5
\end{bmatrix}; \quad (43)
\end{aligned}$$

$$[\bar{\varepsilon}]_6^0 = [R]_6^0 \cdot [\bar{\varepsilon}]_6^6, [\bar{\varepsilon}]_6^0 = \begin{bmatrix}
\frac{\ddot{q}_5 c q_2 c q_4 - \dot{q}_2 \dot{q}_4 c q_2 - \dot{q}_4 \dot{q}_5 c q_2 s q_4 - \ddot{q}_4 s q_2 - \dot{q}_2 \dot{q}_5 s q_2 c q_4}{\ddot{q}_2 - \dot{q}_5 s q_4 - \dot{q}_4 \dot{q}_5 c q_4} \\
\frac{\ddot{q}_5 s q_2 c q_4 - \dot{q}_2 \dot{q}_4 s q_2 - \dot{q}_4 \dot{q}_5 s q_2 s q_4 + \ddot{q}_4 c q_2 + \dot{q}_2 \dot{q}_5 c q_2 c q_4}{\ddot{q}_2 - \dot{q}_5 s q_4 - \dot{q}_4 \dot{q}_5 c q_4}
\end{bmatrix}. \quad (44)$$

In accordance with [Isp04], relations (41), operational speed and acceleration in fixed (42), (43) and (44), may be expressed system $O_0x_0y_0z_0$. So:

$$\begin{aligned}
[\dot{\bar{X}}]_6^0 &= \begin{bmatrix}
\dot{q}_4 l_7 c q_2 c q_4 s q_5 - \dot{q}_3 s q_2 - \dot{q}_2 l_7 s q_2 s q_4 s q_5 + \dot{q}_5 l_7 s q_2 s q_5 - \dot{q}_2 q_3 c q_2 - l_4 \dot{q}_2 c q_2 - l_5 \dot{q}_2 c q_2 - \\
-l_6 \dot{q}_2 c q_2 + \dot{q}_5 l_7 c q_2 s q_4 c q_5 - \dot{q}_2 l_7 c q_2 c q_5 \\
\hline
\dot{q}_3 c q_2 - \dot{q}_5 l_7 c q_2 s q_5 - \dot{q}_2 q_3 s q_2 - l_4 \dot{q}_2 s q_2 - l_5 \dot{q}_2 s q_2 - l_6 \dot{q}_2 s q_2 + \dot{q}_4 l_7 s q_2 c q_4 s q_5 + \\
+ \dot{q}_2 l_7 c q_2 s q_4 s q_5 + \dot{q}_5 l_7 s q_2 s q_4 c q_5 - \dot{q}_2 l_7 s q_2 c q_5 \\
\hline
\dot{q}_1 - \dot{q}_4 l_7 s q_4 s q_5 + \dot{q}_5 l_7 c q_5 c q_4 \\
\hline
\dot{q}_5 c q_2 c q_4 - \dot{q}_4 s q_2 \\
\dot{q}_5 s q_2 c q_4 + \dot{q}_4 c q_2 \\
\dot{q}_2 - \dot{q}_5 s q_4
\end{bmatrix}; \quad (45)
\end{aligned}$$

$$\left[\ddot{\mathbf{X}} \right]^p = \left[\begin{array}{l}
 -\ddot{q}_3sq_2 - \ddot{q}_2l_7sq_2sq_5sq_4 - 2\dot{q}_2\dot{q}_4l_7sq_2sq_5cq_4 + \ddot{q}_5l_7cq_2sq_4cq_5 + \ddot{q}_5l_7sq_2sq_5 + \\
 + 2\dot{q}_2\dot{q}_5l_7cq_2sq_5 + \dot{q}_5^2l_7sq_2cq_5 + \dot{q}_2^2l_5sq_2 + q_3\dot{q}_2^2sq_2 + \dot{q}_2^2l_4sq_2 - \\
 - \ddot{q}_2l_6cq_2 - \ddot{q}_2l_7cq_2cq_5 - q_3\ddot{q}_2cq_2 - \ddot{q}_2l_4cq_2 - \dot{q}_4^2l_7cq_2sq_4sq_5 - \\
 - \dot{q}_2^2l_7cq_2sq_4sq_5 - 2\dot{q}_2\dot{q}_3cq_2 - \ddot{q}_5l_5cq_2 + \dot{q}_2^2l_7sq_2cq_5 + \dot{q}_2^2l_6sq_2 - \\
 - 2\dot{q}_2\dot{q}_5l_7sq_2cq_5sq_4 + \ddot{q}_4l_7cq_2cq_4sq_5 + 2\dot{q}_4\dot{q}_5l_7cq_2cq_4cq_5 - \dot{q}_5^2l_7cq_2sq_4sq_5 \\
 - \ddot{q}_2l_6sq_2 - \dot{q}_2^2l_7cq_2cq_5 - q_3\ddot{q}_2sq_2 - \dot{q}_4^2l_7sq_2sq_4sq_5 + 2\dot{q}_2\dot{q}_5l_7sq_2sq_5 - \\
 - \dot{q}_2^2l_7sq_2sq_4sq_5 - \dot{q}_2^2l_6cq_2 - 2\dot{q}_2\dot{q}_3sq_2 - \ddot{q}_2l_4sq_2 - \dot{q}_2^2l_4cq_2 - \ddot{q}_5l_5sq_2 - \\
 - \ddot{q}_2l_7sq_2cq_5 - \dot{q}_2^2l_5cq_2 - q_3\dot{q}_2^2cq_2 + \ddot{q}_3cq_2 - \dot{q}_2^2l_7cq_2cq_5 - \ddot{q}_5l_7cq_2sq_5 + \\
 + \ddot{q}_4l_7sq_2cq_4sq_5 + 2\dot{q}_4\dot{q}_5l_7sq_2cq_4cq_5 + 2\dot{q}_2\dot{q}_5l_7cq_2cq_5sq_4 - \dot{q}_5^2l_7sq_2sq_4sq_5 + \\
 + \ddot{q}_2l_7cq_2sq_5sq_4 + 2\dot{q}_2\dot{q}_4l_7cq_2sq_5cq_4 + \ddot{q}_5l_7sq_2sq_4cq_5 \\
 \hline
 \ddot{q}_1 + g - \dot{q}_4^2l_7cq_4sq_5 - \ddot{q}_4l_7sq_4sq_5 - \dot{q}_5^2l_7cq_4sq_5 - 2\dot{q}_4\dot{q}_5l_7sq_4cq_5 + \ddot{q}_5l_7cq_4cq_5 \\
 \hline
 \frac{\ddot{q}_5cq_2cq_4 - \dot{q}_2\dot{q}_4cq_2 - \dot{q}_4\dot{q}_5cq_2sq_4 - \ddot{q}_4sq_2 - \dot{q}_2\dot{q}_5sq_2cq_4}{\ddot{q}_5sq_2cq_4 - \dot{q}_2\dot{q}_4sq_2 - \dot{q}_4\dot{q}_5sq_2sq_4 + \ddot{q}_4cq_2 + \dot{q}_2\dot{q}_5cq_2cq_4} \\
 \hline
 \ddot{q}_2 - \ddot{q}_5sq_4 - \dot{q}_4\dot{q}_5cq_4
 \end{array} \right] \quad (46)$$

3. CONCLUSIONS

Equations (39), (40), (45) and (46) are direct kinematics model equations with which can be determined the kinematics operational parameters of the prehensiune device in relation to the reference systems (T₆) and (T₀).

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MODELUL CINEMATIC DIRECT AL ROBOTULUI SERIAL MODULAR TRTRR

Rezumat: Lucrarea prezintă modelarea cinematică a unui robot serial modular cu cinci grade de mobilitate, care este compus din trei module de rotație și două de translație. Robotul, astfel conceput, face parte dintr-o celulă de fabricație, pentru care structura este impusă de mișcările necesare din punct de vedere funcțional, pentru încadrarea în structura propusă. În această lucrare se propune modelarea cinematică a robotului TRTRR, care este continuarea firească a modelării geometrice.

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